

Benchmark on the numerical simulation of a tube bundle vibration under cross flow

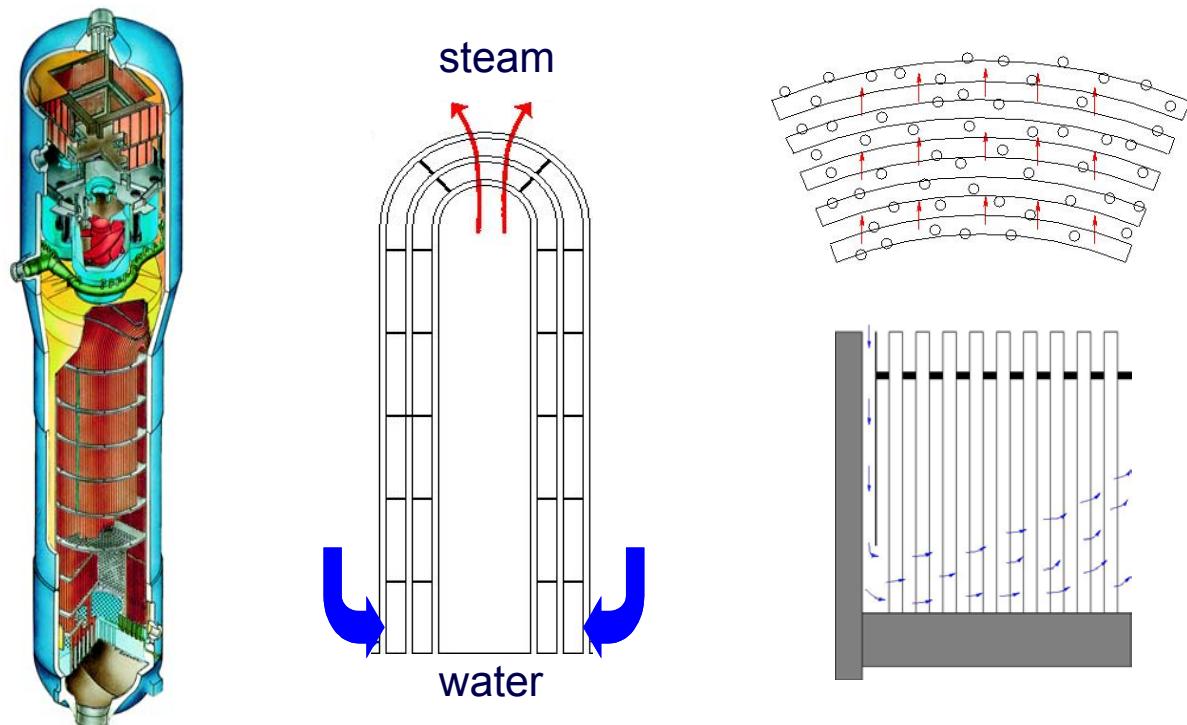
Fabien Huvelin (University of Lille & EDF R&D)

Marcus Vinicius Girao de Morais (University of Cergy-Pontoise & CEA)
Franck Baj (CEA)
Jean-Paul Magnaud (CEA)
Elisabeth Longatte (EDF R&D)
M'hamed Souli (University of Lille)

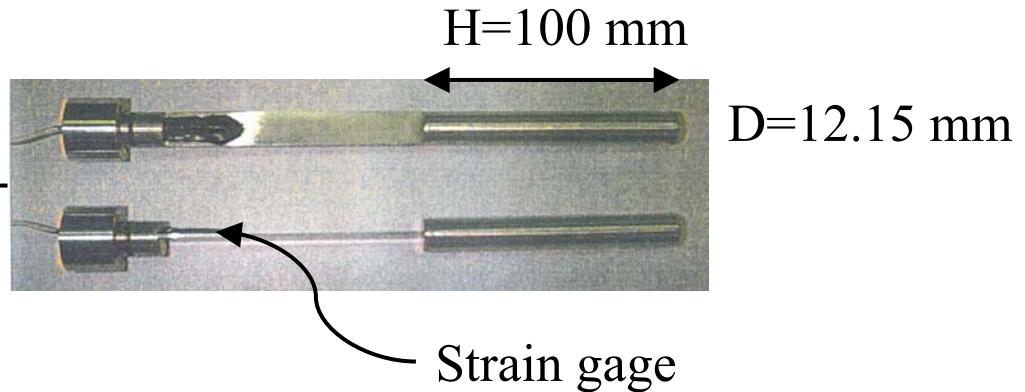
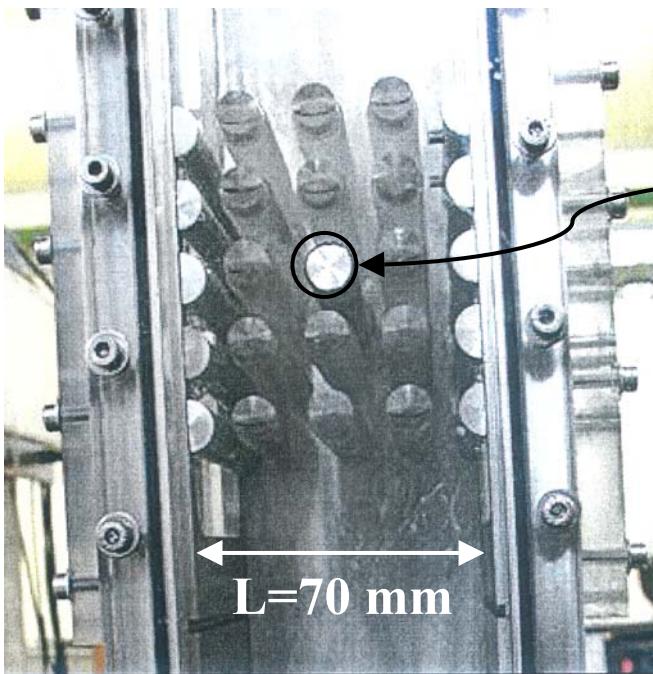
INTRODUCTION

CREATIF Program :

Comprehension of the vibratory Response of an Array of Tubes in Interaction with a Fluid.



Experiment AMOVI (CEA)



- 24 fixed tubes (Plexiglas, $f > 300 \text{ Hz}$)
- 1 moving tube (steel, $f = 14.3 \text{ Hz}$)
- $P/D = 1.44$
- Single phase flow (flow rate from 0 to $5 \text{ m}^3 \cdot \text{h}^{-1}$)

contact : fbaj@cea.fr

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2 – Real case (2D model)

3 – Numerical case (2D model)

4 – Real case (3D model)

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Methodology

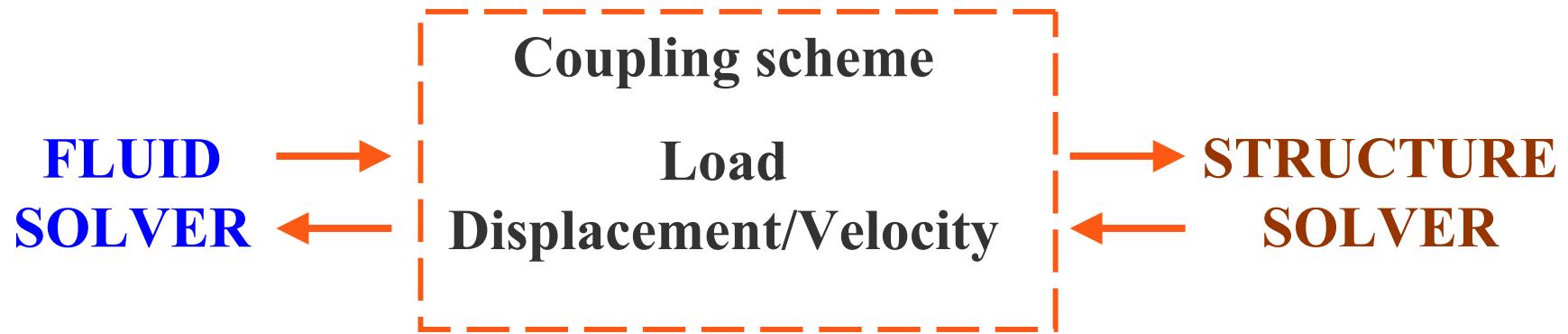
1.1 Boundary conditions

METHODOLOGY | REAL CASE (2D MODEL) | NUMERICAL CASE (2D MODEL) | REAL CASE (3D MODEL)

Boundary conditions at fluid-structure interface

$$\begin{cases} \overline{\overline{u}}_s = \overline{\overline{u}}_f \\ \overline{\sigma}_s \cdot \vec{n} = \overline{\sigma}_f \cdot \vec{n} \end{cases}$$

Partitioned coupling



1.2 Tools

METHODOLOGY | REAL CASE (2D MODEL) | NUMERICAL CASE (2D MODEL) | REAL CASE (3D MODEL)

Structure solver (rigid body)

- 1 degree of freedom oscillator for EDF tool
- Finite element method with Lagrangian formulation for CEA tool

Fluid solver

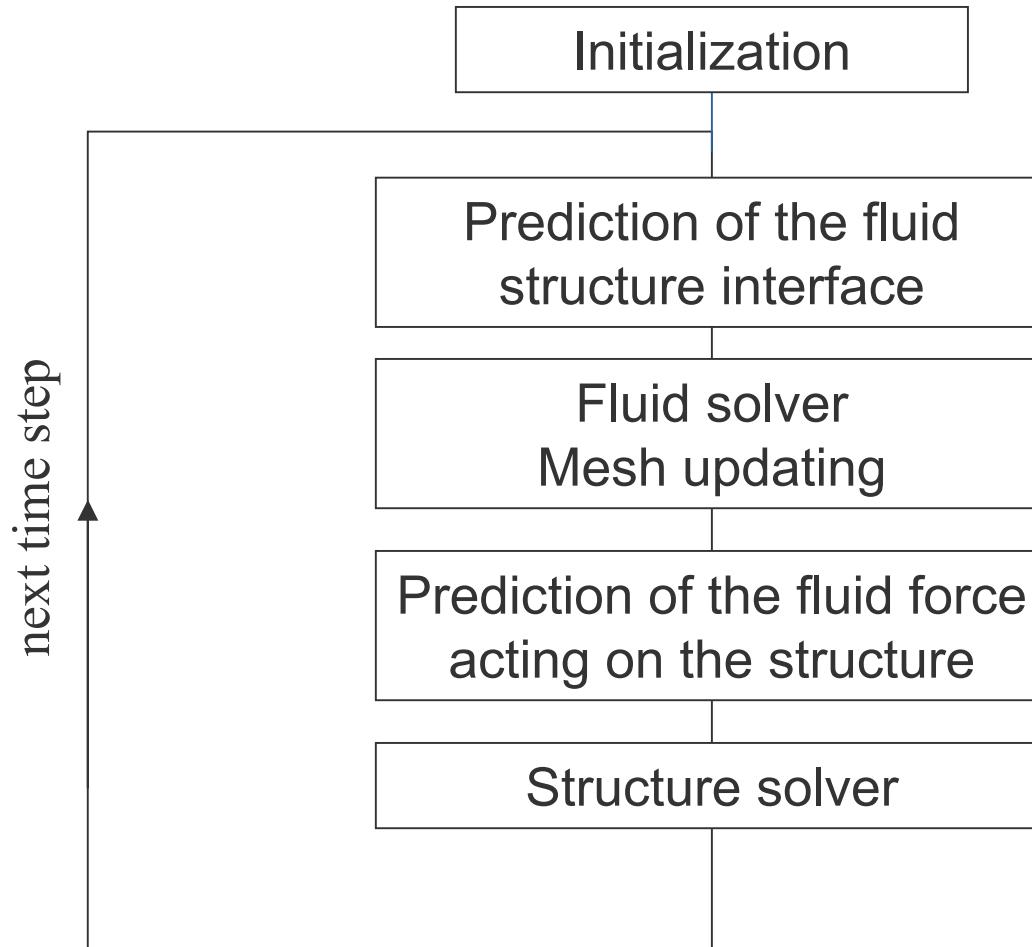
- Finite volume method with Eulerian formulation (EDF tool)
- Finite element method with Eulerian formulation (CEA tool)
⇒ Use of an ALE technique to follow the structure interface (both cases)

Partitioned procedure

- Fluid solver needs structure data at time t^{n+1}
- Structure solver needs fluid data at time t^{n+1}
⇒ Prediction : the position of the structure interface at time t^{n+1}

1.3 Improved serial staggered procedure

METHODOLOGY | REAL CASE (2D MODEL) | NUMERICAL CASE (2D MODEL) | REAL CASE (3D MODEL)



$$X_{\text{fluid}}^{\text{pred},n+1} = X_{\text{structure}}^n + \frac{\Delta t}{2} V_{\text{structure}}^n$$

$$F_{\text{structure}}^{\text{pred},n+1} = 2F_{\text{fluid}} - F_{\text{structure}}^{\text{pred},n}$$

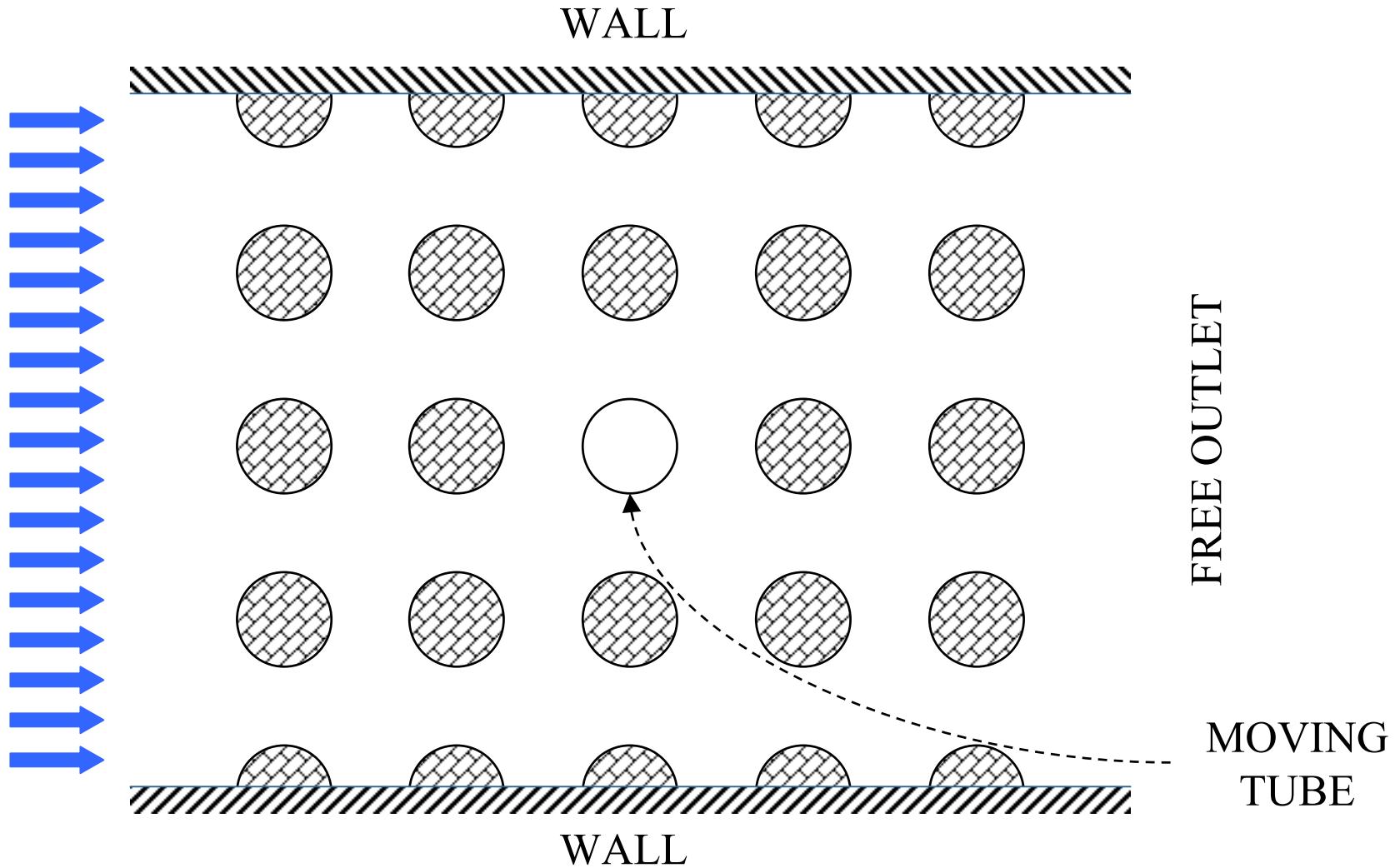
(Piperno et al. ,2001)

2

Real case (2D model)

2.1 Geometry (experiment AMOVI, CEA)

METHODOLOGY | REAL CASE (2D MODEL) | NUMERICAL CASE (2D MODEL) | REAL CASE (3D MODEL)

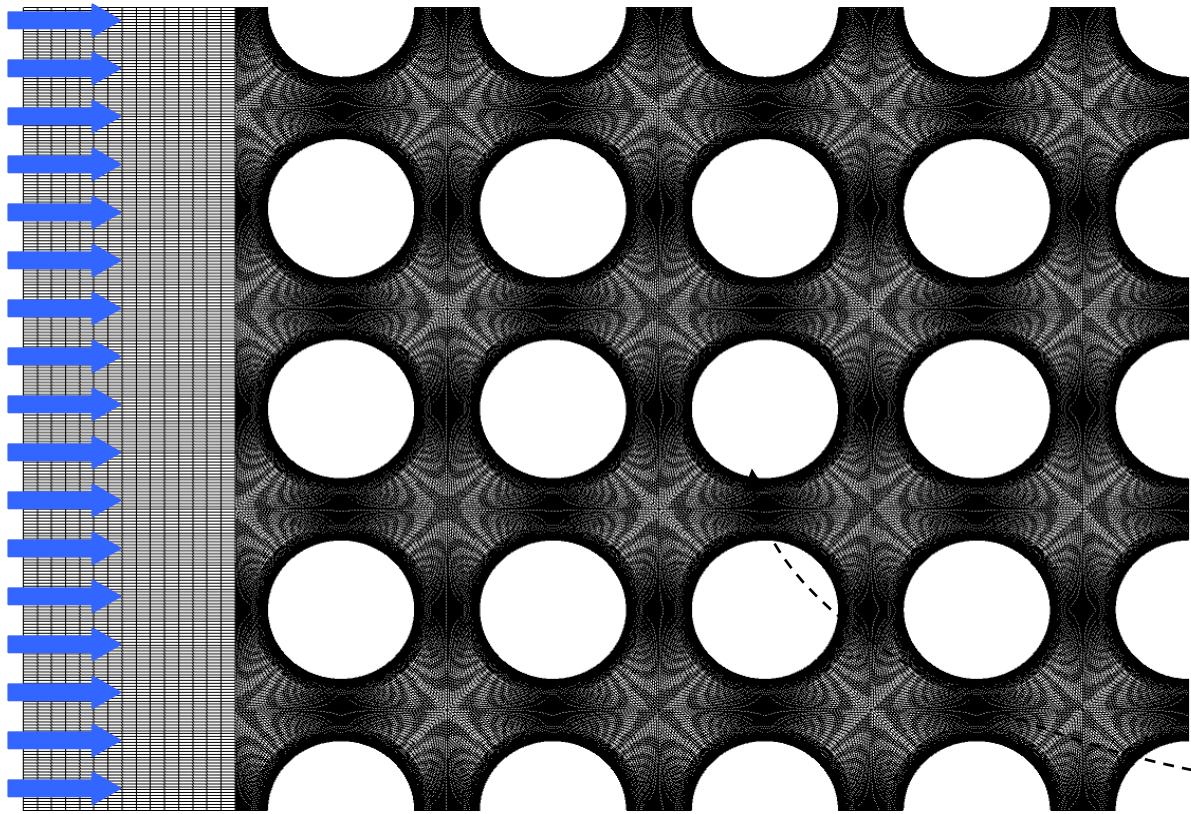


2.1 Geometry (experiment AMOVI, CEA)

METHODOLOGY | REAL CASE (2D MODEL) | NUMERICAL CASE (2D MODEL) | REAL CASE (3D MODEL)

WALL

INLET FLOW



FREE OUTLET

MOVING
TUBE

WALL

2.2 Parameters

METHODOLOGY | REAL CASE (2D MODEL) | NUMERICAL CASE (2D MODEL) | REAL CASE (3D MODEL)

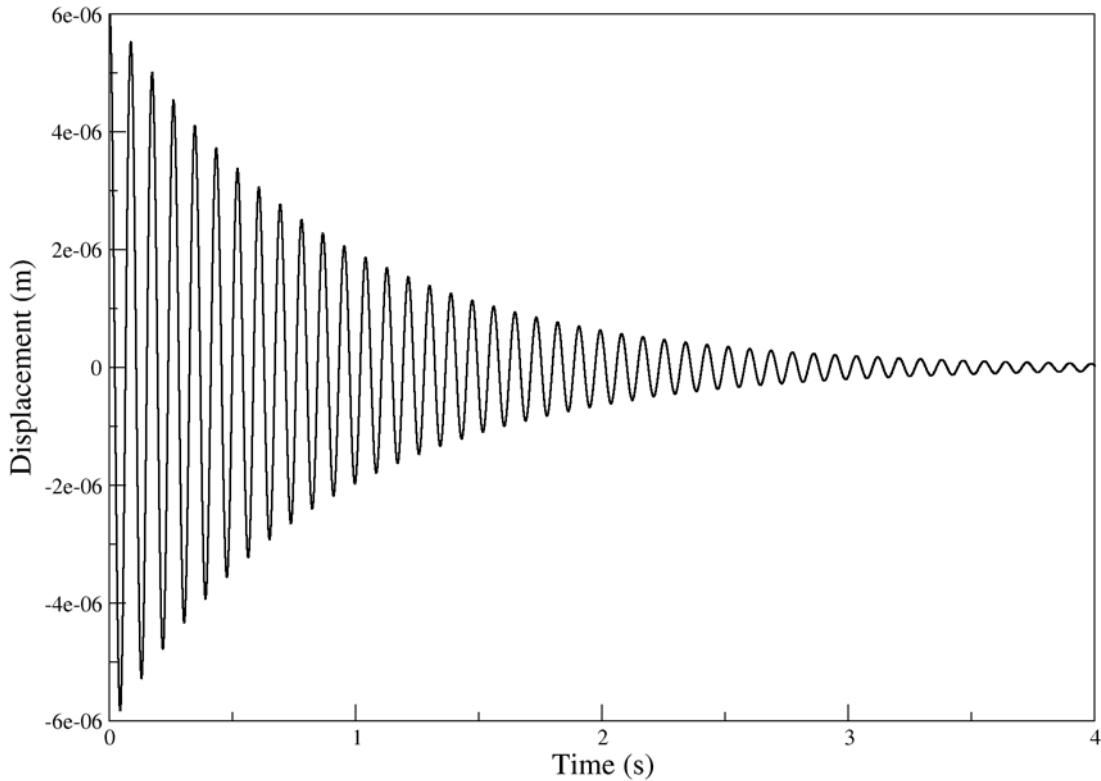
<i>Structure properties</i>		
Natural frequency	(Hz)	14.3
Natural damping	(%)	0.25
Mass	(kg.m ⁻¹)	0.298
Diameter	(mm)	12.15

<i>Fluid properties</i>		
Density	(kg.m ⁻³)	10 ³
Dynamic viscosity	(kg.m ^{-1.s⁻¹)}	10 ⁻³

P/D	(-)	1.44
Inlet velocity	(m.s ⁻¹)	[0.03 ; 0.15]
Reduced velocity	(-)	[0.5 ; 2.8]
Reynolds number	(-)	[1200;6000]

2.3 Quiescent fluid : water frequency

METHODOLOGY | REAL CASE (2D MODEL) | NUMERICAL CASE (2D MODEL) | REAL CASE (3D MODEL)

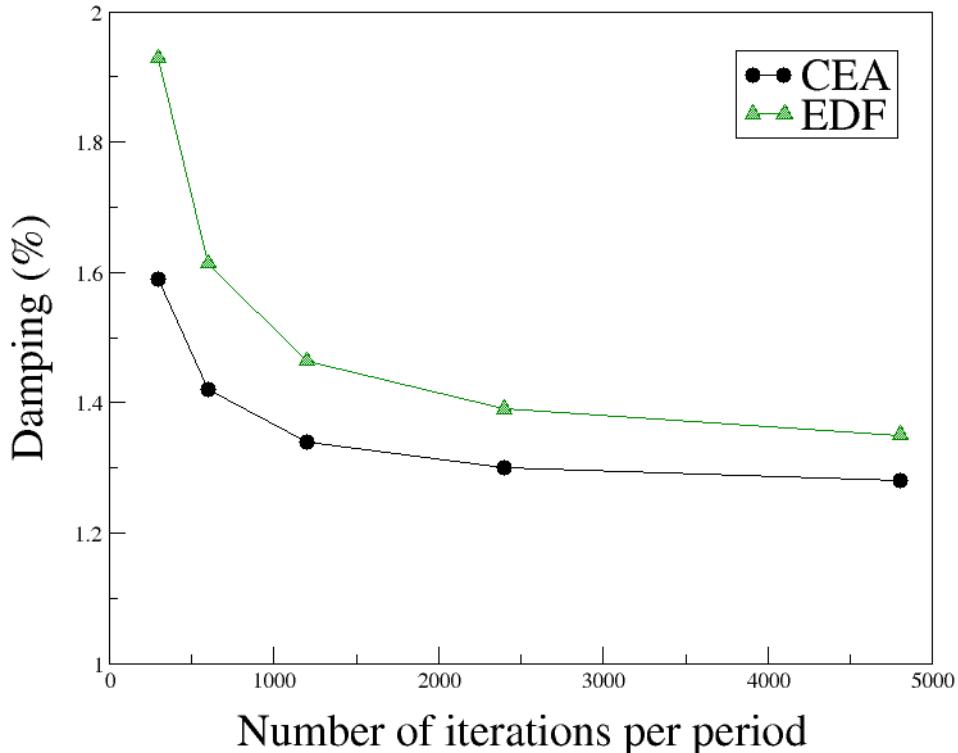


Water
frequency (Hz)

	CEA	EDF	Analytical
Water frequency (Hz)	11.63	11.55	11.8

2.4 Quiescent fluid : water damping

METHODOLOGY | REAL CASE (2D MODEL) | NUMERICAL CASE (2D MODEL) | REAL CASE (3D MODEL)



extrapolation

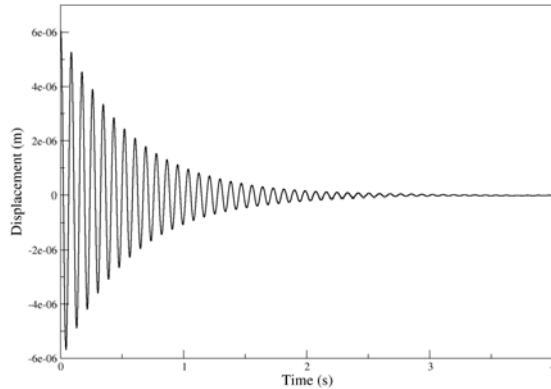
extrapolation	CEA	EDF	Analytical
Water damping (%)	1.216	1.215	1.18

Water damping (%)

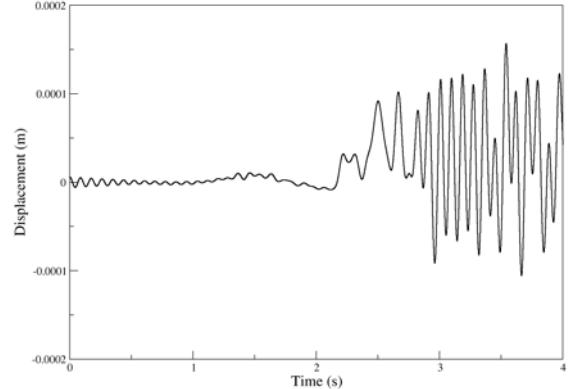
	CEA	EDF	Analytical
Water damping (%)	1.216	1.215	1.18

2.5 Vibration under cross-flow

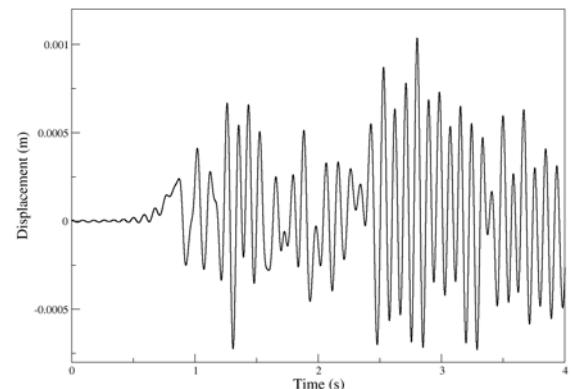
METHODOLOGY | REAL CASE (2D MODEL) | NUMERICAL CASE (2D MODEL) | REAL CASE (3D MODEL)



$Re = 1200$



$Re = 3000$



$Re = 4800$

- Numerical problem ?
- Physical problem ?

3

Numerical case (2D model)

3.1 Parameters

METHODOLOGY | REAL CASE (2D MODEL) | NUMERICAL CASE (2D MODEL) | REAL CASE (3D MODEL)

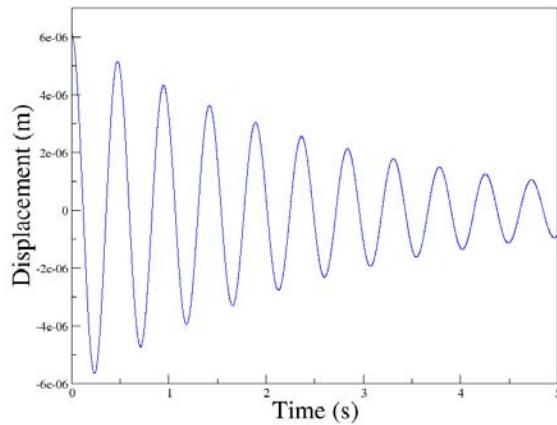
<i>Structure properties</i>	
Natural frequency	(Hz)
2.5	
Natural damping	(%)
0.0437	
Mass	(kg)
0.298	
Diameter	(mm)
10.00	

<i>Fluid properties</i>	
Density	(kg.m ⁻³)
10 ³	
Dynamic viscosity	(kg.m ^{-1.s⁻¹})
10 ⁻³	

P/D	(-)	1.44
Inlet velocity	(m.s ⁻¹)	[0.001 ; 0.035]
Reduced velocity	(-)	[0.1 ; 4.5]
Reynolds number	(-)	[30 ; 1200]

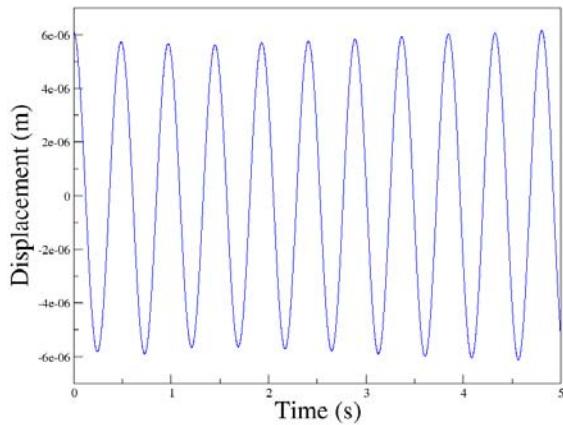
3.2 Displacement

METHODOLOGY | REAL CASE (2D MODEL) | NUMERICAL CASE (2D MODEL) | REAL CASE (3D MODEL)



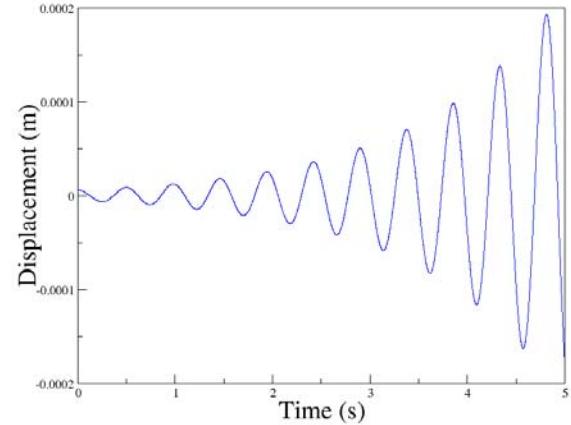
$$v_{inlet} = 0.001 \text{ m.s}^{-1}$$

$$v_{red} = 0.13 (-)$$



$$v_{inlet} = 0.02 \text{ m.s}^{-1}$$

$$v_{red} = 2.62 (-)$$

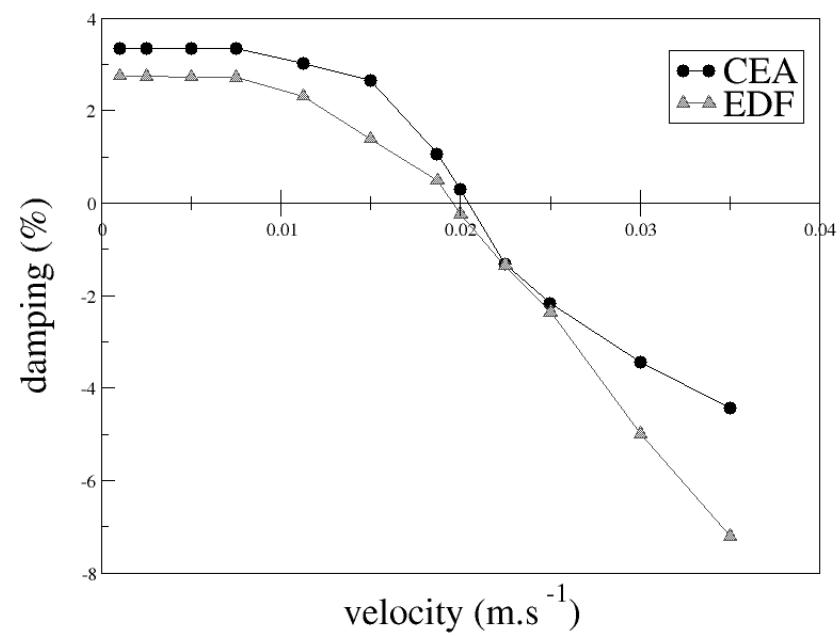
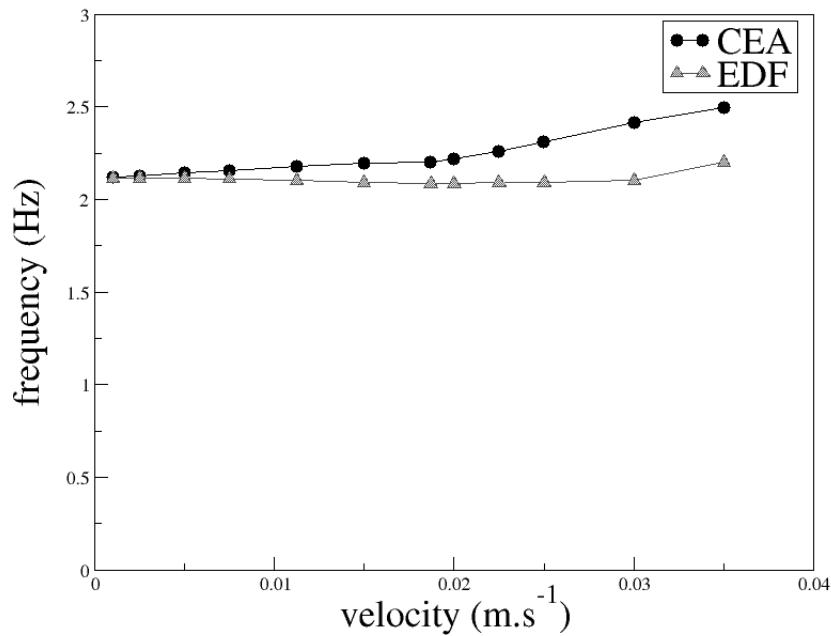


$$v_{inlet} = 0.03 \text{ m.s}^{-1}$$

$$v_{red} = 3.93 (-)$$

3.3 Frequency and damping

METHODOLOGY | REAL CASE (2D MODEL) | NUMERICAL CASE (2D MODEL) | REAL CASE (3D MODEL)

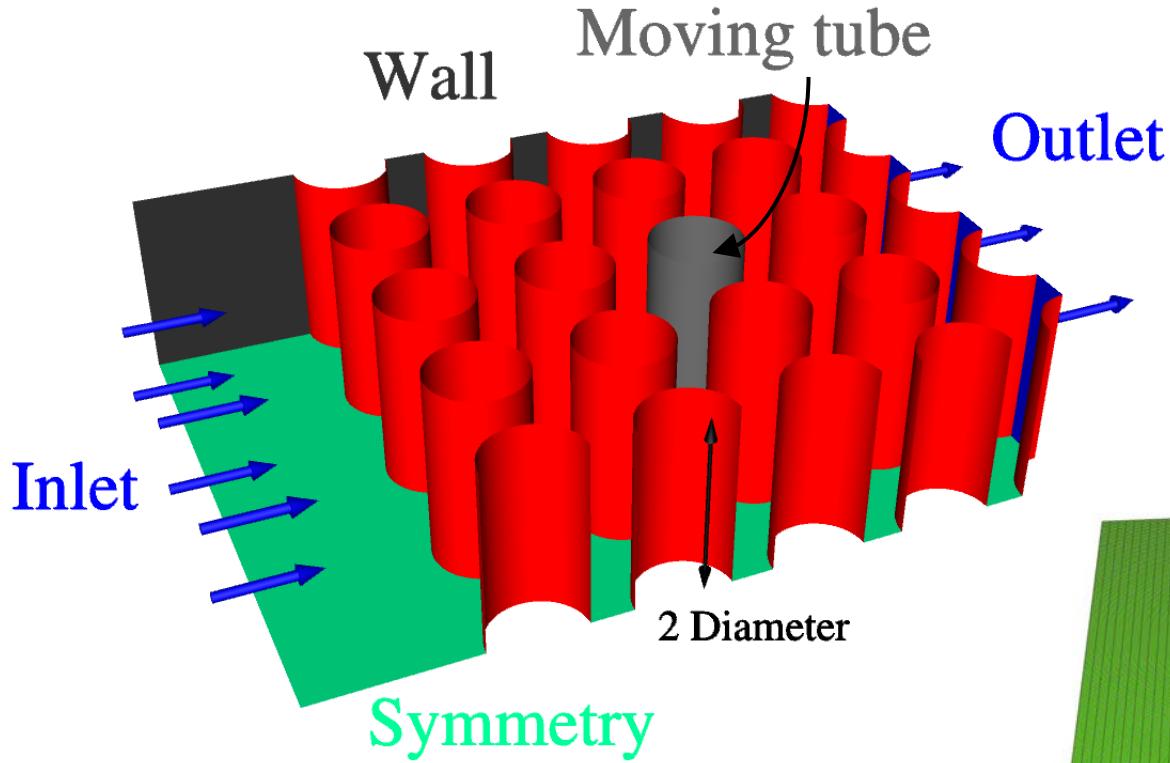


4

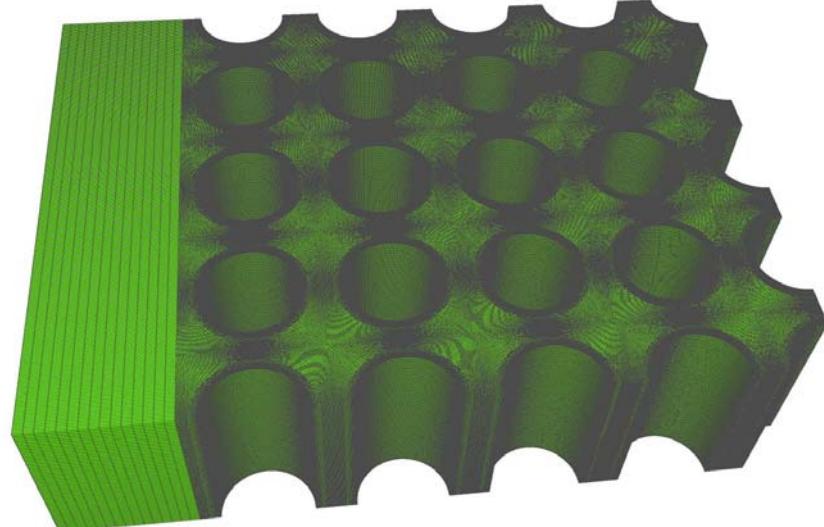
Real case (3D model)

4.1 Geometry

METHODOLOGY | REAL CASE (2D MODEL) | NUMERICAL CASE (2D MODEL) | REAL CASE (3D MODEL)



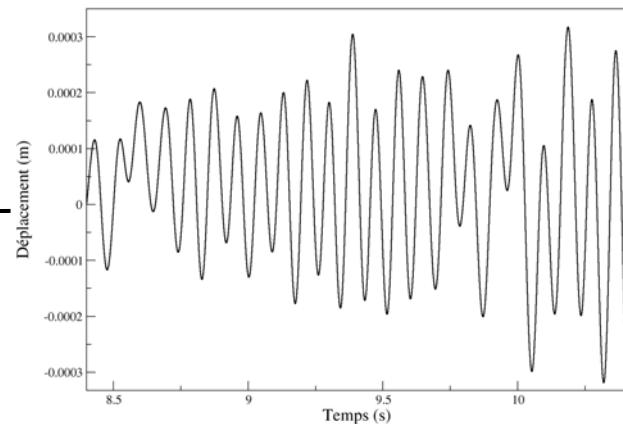
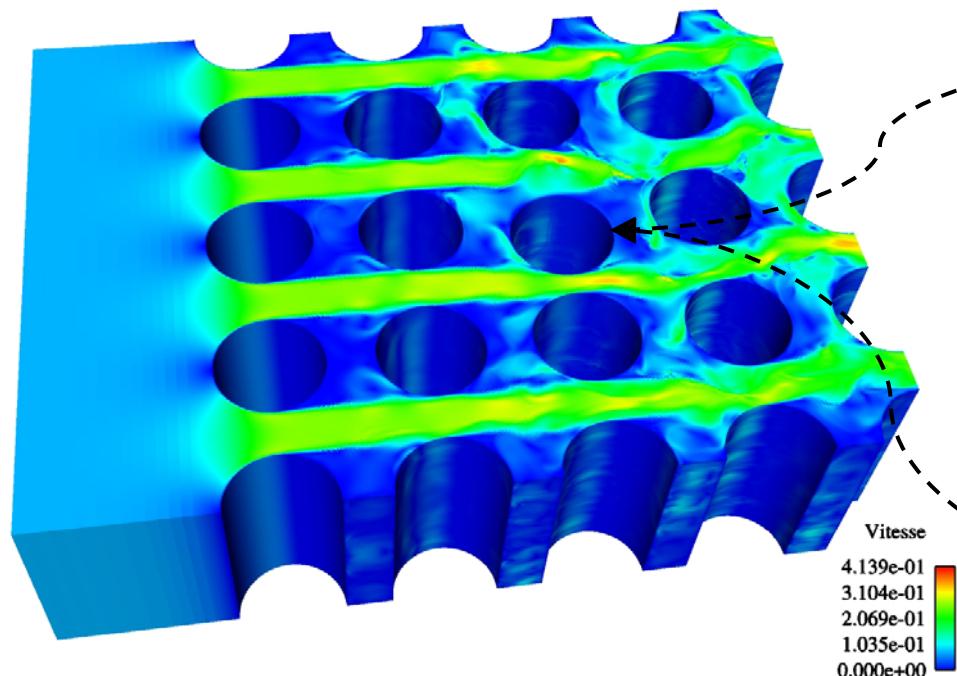
- 7.5 Millions of elements
- 2048 processors



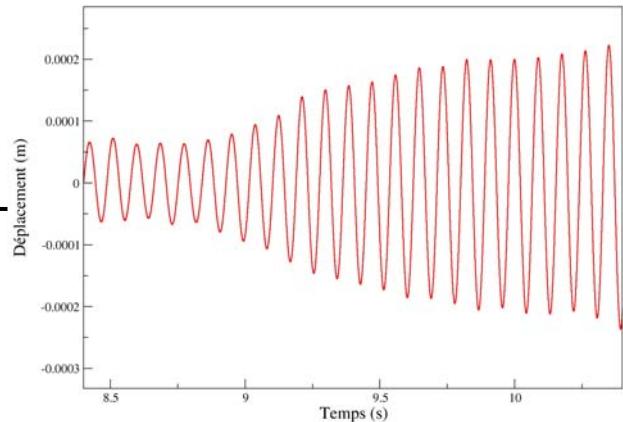
4.2 Preliminary results

METHODOLOGY | REAL CASE (2D MODEL) | NUMERICAL CASE (2D MODEL) | REAL CASE (3D MODEL)

Reynolds = 3000 and DNS



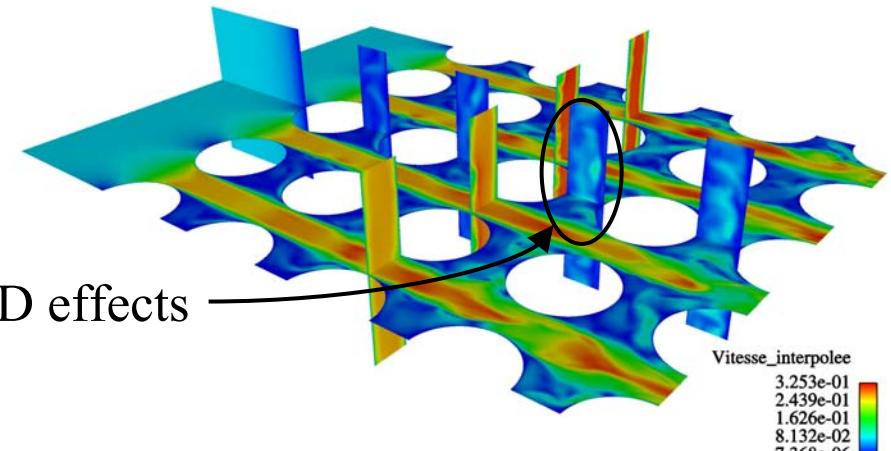
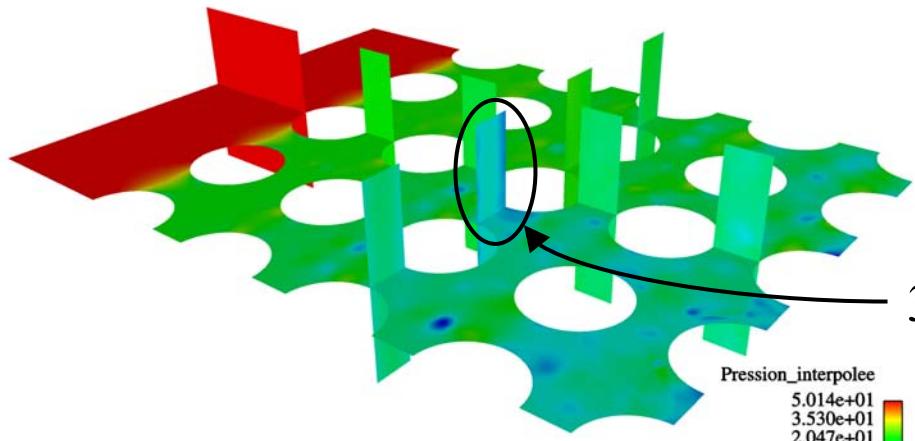
Displacement with 2D simulation



Displacement with 3D simulation

4.3 3D effect

METHODOLOGY | REAL CASE (2D MODEL) | NUMERICAL CASE (2D MODEL) | **REAL CASE (3D MODEL)**



CONCLUSION

- ✓ Catch the 3 behaviors of the structure
 - ✓ Used of an extrapolation method for the damping
 - ✓ Over-estimation of force fluid with 2D simulation
(3D simulation is required)
-
- 3D simulation for numerical case
 - 3D simulation with turbulent model for real case
 - Comparison of the real case to the experiment AMOVI (CEA)